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(54) **PRELOADED DROP HAMMER FOR DRIVING PILES**

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This patent is subject to a terminal disclaimer.

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USPC **173/1**; 173/89; 173/132; 173/212

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USPC 173/1, 89, 132, 133, 135-137, 206, 173/208, 209, 212; 405/232

See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

5,015 A	3/1847	Ingalls
48,515 A	7/1865	Campbell et al.
369,176 A	8/1887	Gerstein
400,209 A	3/1889	Haskins
628,962 A	7/1899	Speer

(Continued)

FOREIGN PATENT DOCUMENTS

DE	4010357	10/1990
EP	0172960	5/1986

(Continued)

OTHER PUBLICATIONS

American Piledriving Equipment, Inc., A series of photographs identified by Reference Nos. APE01147-APE01159, dates from 1990-1993, 13 pages.

(Continued)

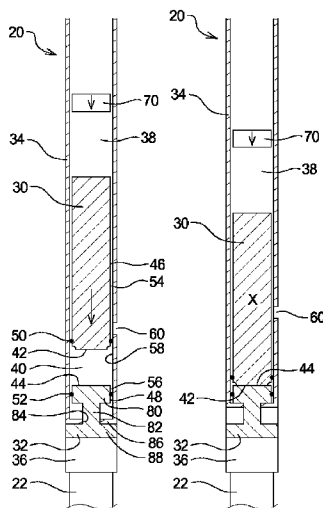
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(57) **ABSTRACT**

A drop hammer for driving a pile comprising a ram member supported within a housing chamber for movement relative to the housing member between the lower position and the upper position and a lifting system for moving the ram member from the lower position to the upper position. When the lifting system raises the ram member above a preload position, ambient air substantially freely flows into and out of the housing chamber through a vent port. When the ram member falls below the preload position, fluid is prevented from flowing through the vent port such that ambient air within a preload chamber portion of the housing chamber compresses to create a preload force that is transmitted to the pile. When the ram member moves into the lower position, an impact force generated by the ram member is transmitted to the pile.

13 Claims, 4 Drawing Sheets



U.S. PATENT DOCUMENTS							
999,334	A	8/1911	Pearson	3,959,557	A	5/1976	Berry
1,128,808	A	2/1915	Manoogian	3,967,688	A	7/1976	Inenaga et al.
1,213,800	A	1/1917	Piper	3,975,918	A	8/1976	Jansz
1,288,989	A	12/1918	Rees	3,991,833	A	11/1976	Ruppert
1,294,154	A	2/1919	Payne	3,998,063	A	12/1976	Harders
1,322,470	A	11/1919	Schenk	4,018,290	A	4/1977	Schmidt
1,348,994	A	8/1920	Heckle	4,029,158	A	6/1977	Gerrish
1,464,231	A	8/1923	Yezeck	4,033,419	A	7/1977	Pennington
1,654,093	A	12/1927	Reid	4,067,369	A	1/1978	Harmon
1,702,349	A	2/1929	Krell	4,076,081	A	2/1978	Schnell
1,748,555	A	2/1930	Kinney	4,082,361	A	4/1978	Lanfermann
1,762,037	A	6/1930	Taylor	4,099,387	A	7/1978	Frederick et al.
1,769,169	A	7/1930	Thornley	4,100,974	A	7/1978	Pepe
1,787,000	A	12/1930	Hunt	4,102,408	A	7/1978	Ludvigson
1,903,555	A	4/1933	Robertson	4,109,475	A	8/1978	Schnell
1,914,899	A	6/1933	Syme	4,113,034	A	9/1978	Carlson
1,988,173	A	1/1935	Kersting	4,119,159	A	10/1978	Arentsen
2,068,045	A	1/1937	Wohlmeyer	4,143,985	A	3/1979	Axelsson et al.
2,239,024	A	4/1941	Vance	4,154,307	A	5/1979	Gendron et al.
2,577,252	A	12/1951	Kjellman	4,155,600	A	5/1979	Lanfermann et al.
2,723,532	A	11/1955	Smith	4,166,508	A	9/1979	van den Berg
2,755,783	A	7/1956	Kupka	4,180,047	A	12/1979	Bertelson
2,842,972	A	7/1958	Houdart	4,187,917	A	2/1980	Bouyoucos
2,859,628	A	11/1958	Arko	4,195,698	A	4/1980	Nakagawasai
2,904,964	A	9/1959	Kupka	4,248,550	A	2/1981	Blaschke et al.
2,952,132	A	9/1960	Urban	4,262,755	A	4/1981	Kuhn
3,001,515	A	9/1961	Haaga	4,274,761	A	6/1981	Boguth
3,004,389	A	10/1961	Muller	4,312,413	A	1/1982	Loftis
3,034,304	A	5/1962	Upson	4,362,216	A	12/1982	Jansz
3,094,007	A	6/1963	Luhrs	4,366,870	A	1/1983	Frederick
3,100,382	A	8/1963	Muller	4,375,927	A	3/1983	Kniep
3,101,552	A	8/1963	Tandler	4,380,918	A	4/1983	Killop
3,106,258	A	10/1963	Muller	4,397,199	A	8/1983	Jahn
3,115,198	A	12/1963	Kuss	4,421,180	A	12/1983	Fleishman et al.
3,149,851	A	9/1964	Adams	4,428,699	A	1/1984	Juhola
3,172,485	A	3/1965	Spannhake et al.	4,430,024	A	2/1984	Guild et al.
3,177,029	A	4/1965	Larson	4,455,105	A	6/1984	Juhola
3,193,026	A	7/1965	Kupka	4,465,145	A	8/1984	Kuhn
3,227,483	A	1/1966	Guild et al.	4,497,376	A	2/1985	Kurylko
3,243,190	A	3/1966	Peregrine	4,505,614	A	3/1985	Anschutz
3,267,677	A	8/1966	Bollar	4,519,729	A	5/1985	Clarke, Jr. et al.
3,289,774	A	12/1966	Bodine, Jr.	4,537,527	A	8/1985	Juhola et al.
3,300,987	A	1/1967	Maeda	4,547,110	A	10/1985	Davidson
3,313,376	A	4/1967	Holland, Sr.	4,553,443	A	11/1985	Rossfelder et al.
3,371,727	A	3/1968	Belousov et al.	4,601,615	A	7/1986	Cavalli
3,381,422	A	5/1968	Olson	4,603,748	A	8/1986	Rossfelder et al.
3,391,435	A	7/1968	Lebelle	4,624,325	A	11/1986	Steiner
3,394,766	A	7/1968	Lebelle	4,626,138	A	12/1986	Boyes
3,412,813	A	11/1968	Johnson	4,627,768	A	12/1986	Thomas et al.
3,447,423	A	6/1969	Henry	4,632,602	A	12/1986	Hovnanian
3,450,398	A	6/1969	Barnes	4,637,475	A	1/1987	England et al.
3,460,637	A	8/1969	Schulin	4,645,017	A	2/1987	Bodine
3,513,587	A	5/1970	Fischer	4,687,026	A	8/1987	Westman
3,530,947	A	9/1970	Gendron et al.	4,725,167	A	2/1988	Merjan
3,577,645	A	5/1971	Zurawski	4,735,270	A	4/1988	Fenyvesi
3,583,497	A	6/1971	Kussowski et al.	4,755,080	A	7/1988	Cortlever et al.
3,616,453	A	10/1971	Philpot	4,757,809	A	7/1988	Koeneman et al.
3,620,137	A	11/1971	Prasse	4,758,148	A	7/1988	Jidell
3,638,738	A	2/1972	Varnell	4,768,900	A	9/1988	Burland
3,679,005	A	7/1972	Inaba et al.	4,799,557	A	1/1989	Jacquemet
3,684,037	A	8/1972	Bodine	4,813,814	A	3/1989	Shibuta et al.
3,686,877	A	8/1972	Bodin	4,844,661	A	7/1989	Martin et al.
3,711,161	A	1/1973	Proctor et al.	4,863,312	A	9/1989	Cavalli
3,720,435	A	3/1973	Leyn	4,915,180	A	4/1990	Schisler
3,734,209	A	5/1973	Haisch et al.	4,961,471	A	10/1990	Ovens
3,786,874	A	1/1974	Jodet et al.	4,974,997	A	12/1990	Sero et al.
3,789,930	A	2/1974	Nishimura et al.	4,989,677	A	2/1991	Lam
3,797,585	A	3/1974	Ludvigson	4,993,500	A	2/1991	Greene et al.
3,822,969	A	7/1974	Kummel	5,004,055	A	4/1991	Porritt et al.
3,828,864	A	8/1974	Haverkamp et al.	5,018,251	A	5/1991	Brown
3,854,418	A	12/1974	Bertin	5,076,090	A	12/1991	Cetnarowski
3,861,664	A	1/1975	Durkee	5,088,565	A	2/1992	Evarts
3,865,501	A	2/1975	Kniep	5,107,934	A	4/1992	Atchison
3,871,617	A	3/1975	Majima	5,117,925	A	6/1992	White
3,874,244	A	4/1975	Rasmussen et al.	5,154,667	A	10/1992	Mauch et al.
3,891,186	A	6/1975	Thorsell	5,161,625	A	11/1992	Seng
3,907,042	A	9/1975	Halwas et al.	5,213,449	A	5/1993	Morris
3,952,796	A	4/1976	Larson	5,253,542	A	10/1993	Houze
				RE34,460	E	11/1993	Ishiguro et al.

5,263,544	A	11/1993	White
5,281,775	A	1/1994	Gremillion
5,343,002	A	8/1994	Gremillion
5,355,964	A	10/1994	White
5,375,897	A	12/1994	Gazel-Anthoine
5,385,218	A	1/1995	Migliori
5,409,070	A	4/1995	Roussy
5,410,879	A	5/1995	Houze
5,439,326	A	8/1995	Goughnour et al.
5,540,295	A	7/1996	Serrette
5,544,979	A	8/1996	White
5,549,168	A	8/1996	Sadler et al.
5,562,169	A	10/1996	Barrow
5,609,380	A	3/1997	White
5,653,556	A	8/1997	White
5,658,091	A	8/1997	Goughnour et al.
5,727,639	A	3/1998	Jeter
5,794,716	A	8/1998	White
5,811,741	A	9/1998	Coast et al.
5,836,205	A	11/1998	Meyer
5,860,482	A	1/1999	Gremillion et al.
5,918,511	A	7/1999	Sabbaghian et al.
6,003,619	A	12/1999	Lange
6,039,508	A	3/2000	White
6,056,070	A	5/2000	Shinohara et al.
6,102,133	A	8/2000	Scheid et al.
6,129,159	A	10/2000	Scott et al.
6,129,487	A	10/2000	Birmingham et al.
6,179,527	B1	1/2001	Goughnour
6,186,043	B1	2/2001	Callies
6,216,394	B1	4/2001	Fenelon
6,224,294	B1	5/2001	Mansfield
6,227,767	B1	5/2001	Mosing et al.
6,234,260	B1	5/2001	Coast et al.
6,250,426	B1	6/2001	Lombard
6,360,829	B1	3/2002	Naber et al.
6,364,577	B1	4/2002	Haney
6,386,295	B1	5/2002	Suver
6,427,402	B1	8/2002	White
6,431,795	B2	8/2002	White
6,447,036	B1	9/2002	White
6,543,966	B2	4/2003	White
6,557,647	B2	5/2003	White
6,648,556	B1	11/2003	White
6,672,805	B1	1/2004	White
6,732,483	B1	5/2004	White
6,736,218	B1	5/2004	White
6,896,448	B1	5/2005	White
6,908,262	B1	6/2005	White
6,988,564	B2	1/2006	White
7,168,890	B1	1/2007	Evarts
7,392,855	B1	7/2008	White
7,694,747	B1	4/2010	White
7,708,499	B1	5/2010	Evarts et al.
7,824,132	B1	11/2010	White
7,854,571	B1	12/2010	Evarts
7,950,877	B2	5/2011	Evarts
8,070,391	B2	12/2011	White
8,181,713	B2	5/2012	White
8,186,452	B1	5/2012	White
2010/0303552	A1	12/2010	Yingling et al.
2011/0162859	A1	7/2011	White
2011/0243668	A1	10/2011	White
2011/0252610	A1	10/2011	Evarts
2012/0114424	A1	5/2012	White

FOREIGN PATENT DOCUMENTS

EP	362158	4/1990
EP	526743	10/1993

FR	838717	3/1939
FR	2560247	8/1985
GB	1066727	4/1967
GB	2003769	3/1979
GB	2023496	1/1980
GB	2028902	3/1980
GB	2043755	10/1980
GB	2060742	5/1981
JP	5494703	7/1979
JP	355098526	7/1980
JP	356034828	4/1981
JP	57169130	10/1982
JP	59228529	12/1984
JP	61221416	10/1986
JP	0258627	2/1990
JP	497015	3/1992
JP	473035	6/1992
JP	5246681	9/1993
JP	6136751	5/1994
JP	9328983	12/1997
KR	1020010044658	6/2001
NL	42349	1/1938
NL	65252	2/1950
NL	7710385	3/1978
NL	7707303	1/1979
NL	7805153	11/1979
NO	46428	4/1929
SU	1027357	7/1983
WO	8707673	12/1987
WO	8805843	8/1988

OTHER PUBLICATIONS

APE, "APE Model 8 Hydraulic Impact Hammer," 1 page.

Japan Development Consultants, Inc., "Castle Board Drain Method" Japanese language brochure, Ref. Nos. APE00857-APE00863, Aug. 1976, 7 pages.

International Construction Equipment, Inc., "Diesel Pile Hammers" brochure, Ref. No. DH4-1288-5C, 6 pages.

International Construction Equipment, Inc., "Hydraulic Vibratory Driver/Extractors for Piling and Caisson Work," 10 pages.

International Construction Equipment, Inc., "Hydraulic Vibratory Driver/Extractors for Piling and Caisson Work," Ref. No. V7-0890-51, 3 pages.

"Kony Drain Board," 1994, 1 page.

Korean language documents identified by Ref. Nos. APE00864-APE00891, dates from 1982-1997, 28 pages.

Seibert, www.mmsonline.com/columns/micro-keying-keeps-a-better-grip.aspx, Modern Machine Shop: "Micro-Keying Keeps a Better Grip," Aug. 1, 1992, 2 pages.

MKT Geotechnical Systems, Manual No. 01807: "Operating, Maintenance and Parts manual for MS350 and MS500 Single-Acting Pile Hammers," 12 pages.

Report identifying systems for driving mandrels carrying wick drain material into the earth, Ref. Nos. APE0510-APE0536, 1994, 27 pages.

Schematic drawings, Ref. Nos. APE01038, APE01039, APE0339, 3 pages.

Shanghai Jintai Semw, Portions of Operations Manual for Diesel Hammers Depicting the Basic Operation of Diesel Hammers and Fuel Pumps Used by Commercially Available Diesel Hammers, 8 pages.

"The 1st Report on the Treatment of Soft Foundation in Juck Hyun Industrial Site", Ref. Nos. APE00854-APE00856, 1976, 3 pages.

International Searching Authority, "International Search Report", Nov. 28, 2011, 11 pages.

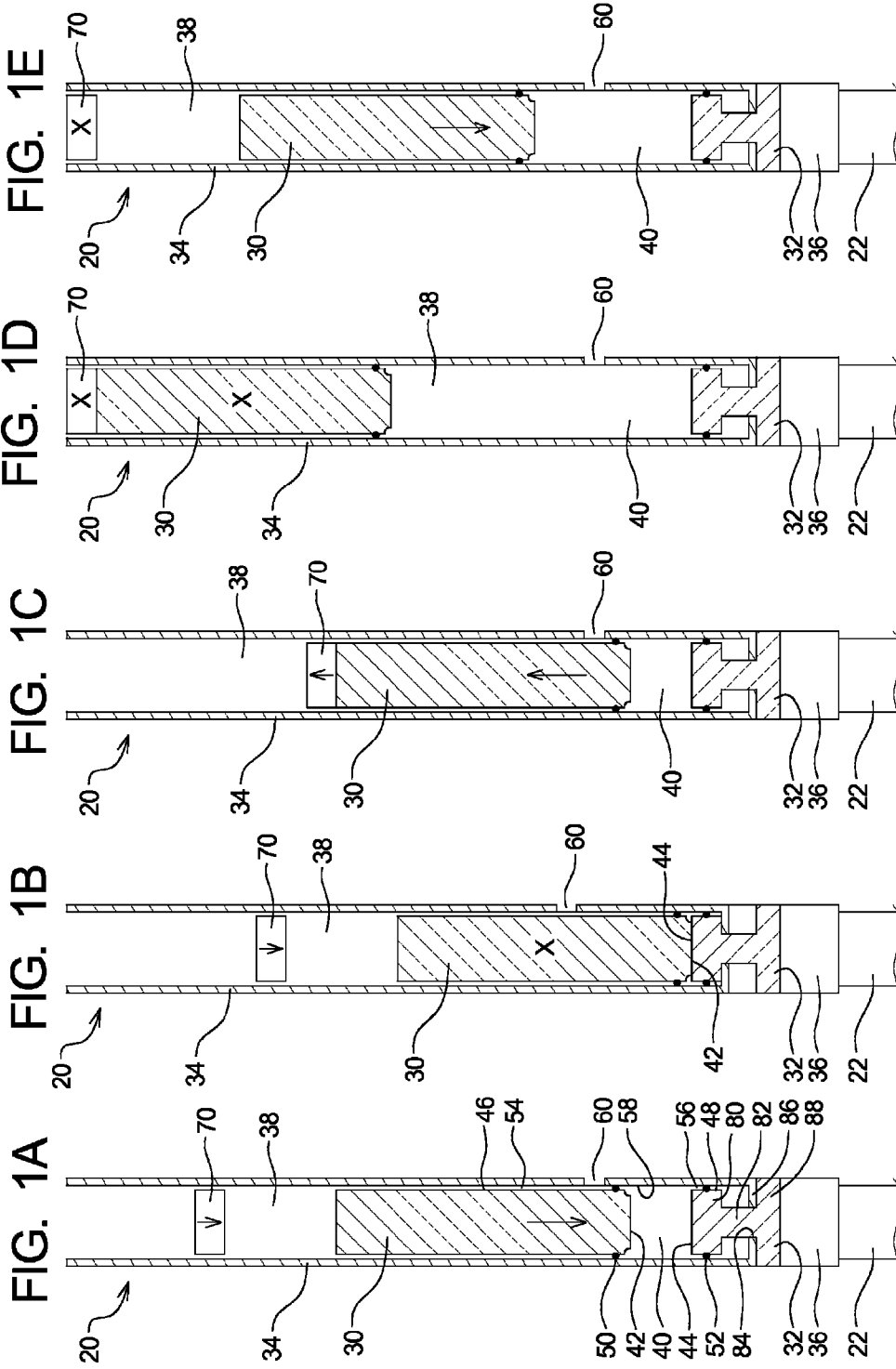


FIG. 2

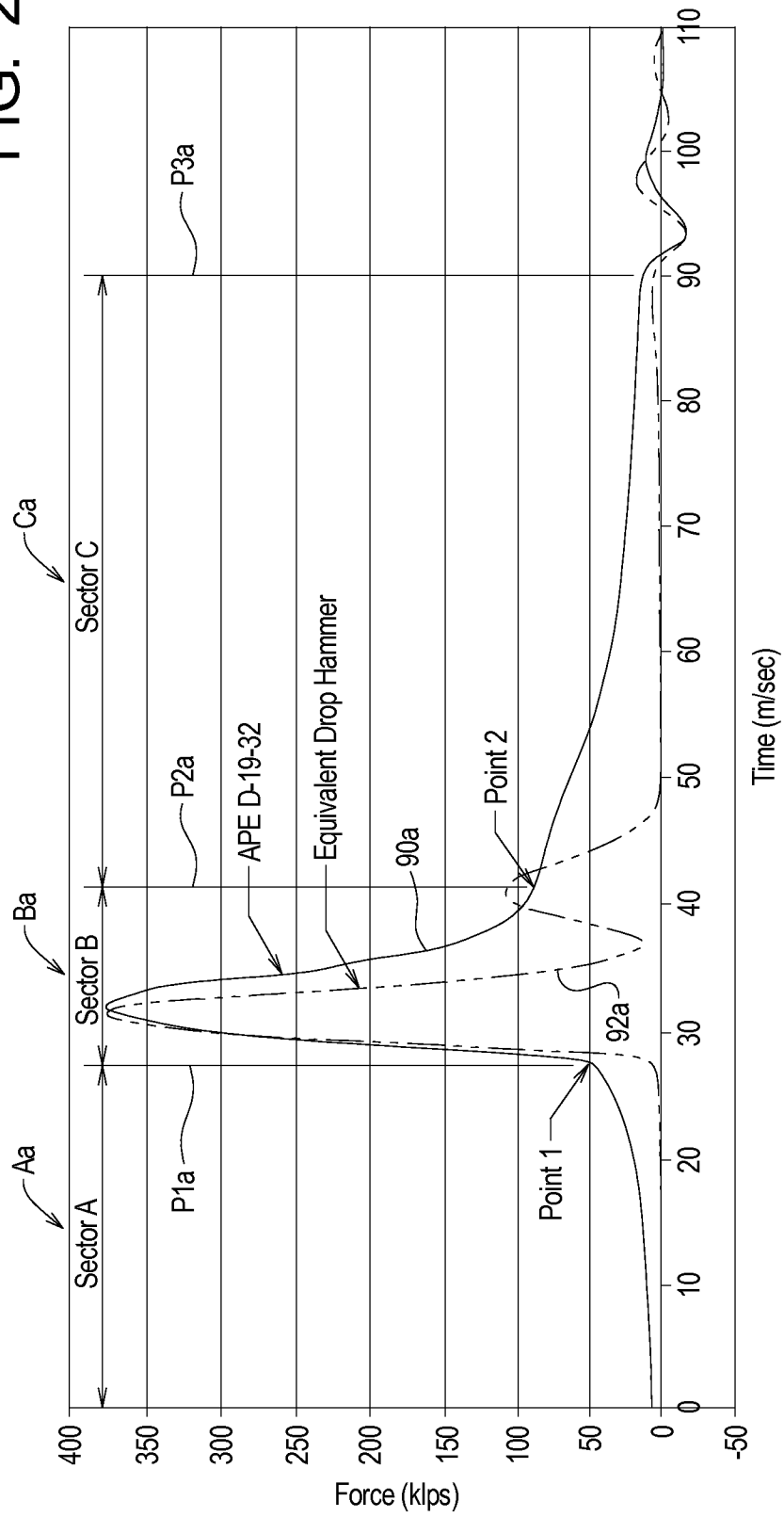


FIG. 3

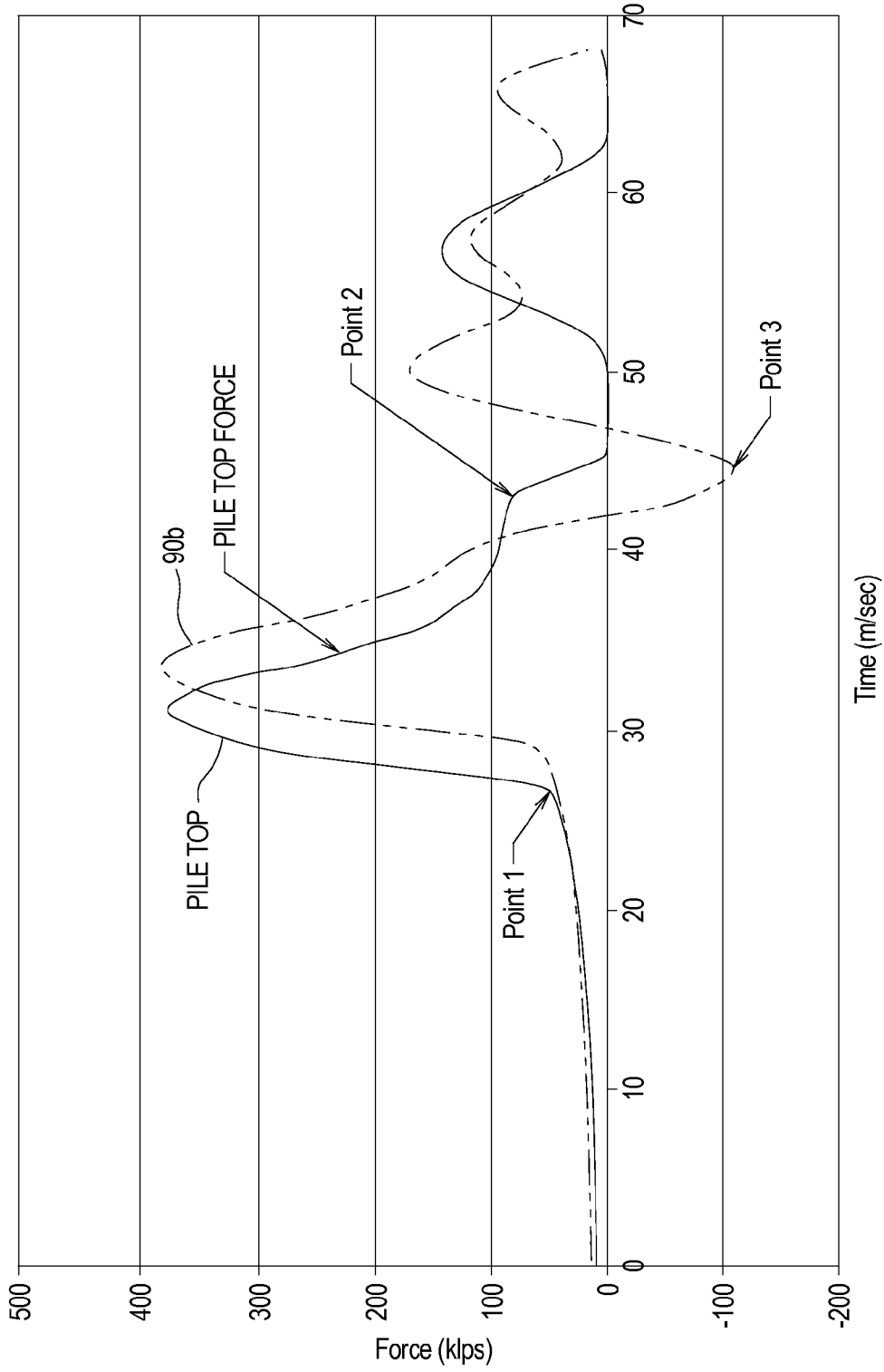
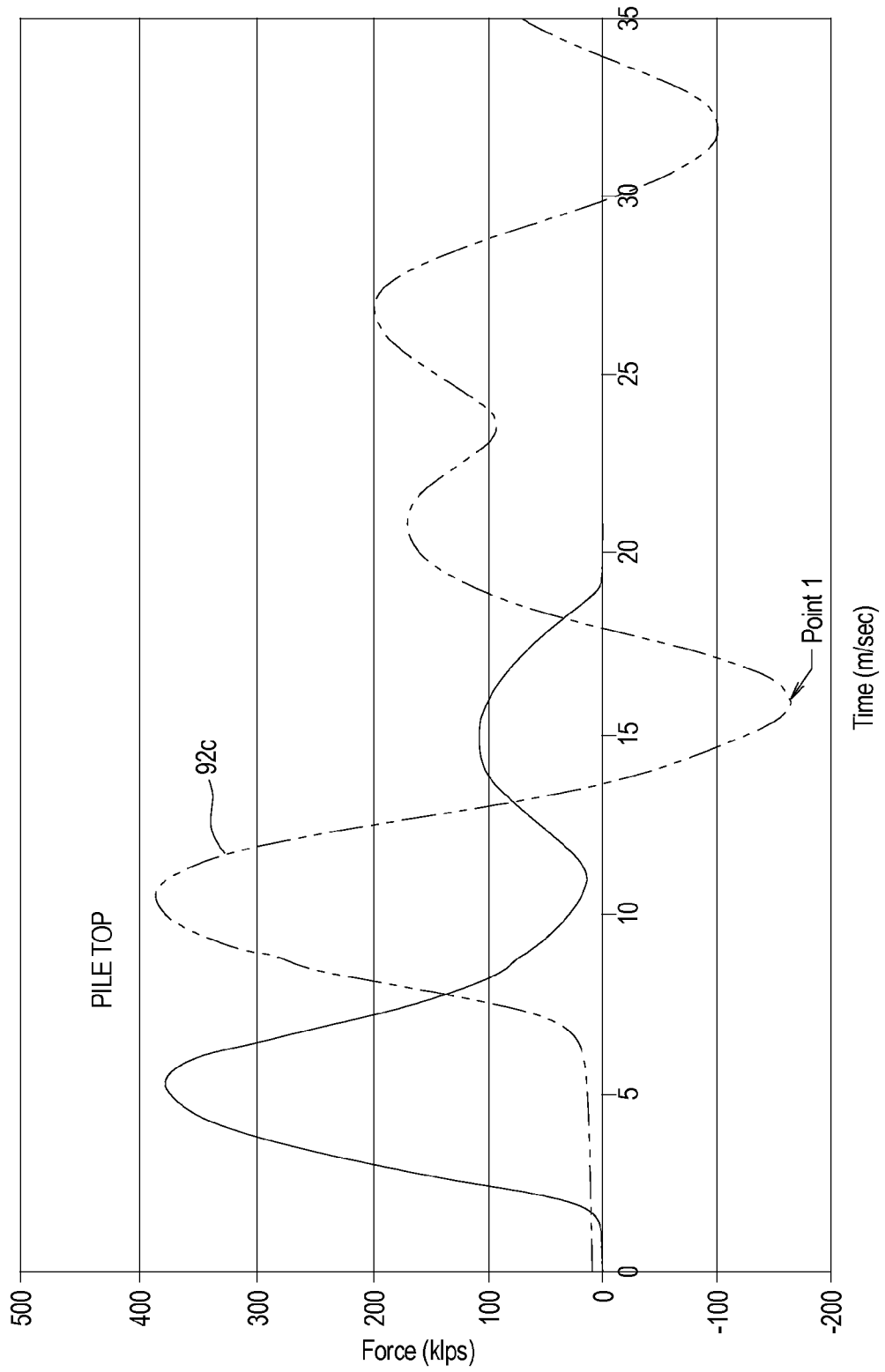


FIG. 4



PRELOADED DROP HAMMER FOR DRIVING PILES

RELATED APPLICATIONS

This application U.S. application Ser. No. 13/477,925, is a continuation of U.S. application Ser. No. 12/758,723, filed Apr. 12, 2010.

U.S. application Ser. No. 12/758,723 is a continuation of U.S. application Ser. No. 10/667,176, filed Sep. 17, 2003, now U.S. Pat. No. 7,694,747, which issued on Apr. 13, 2010.

U.S. application Ser. No. 10/667,176 claims priority of U.S. Provisional application Ser. No. 60/411,683 filed on Sep. 17, 2002.

The contents of all related applications listed above are incorporated herein by reference.

TECHNICAL FIELD

The present invention relates to methods and apparatus for inserting elongate members into the earth and, more particularly, to drop hammers that create pile driving forces by lifting and dropping a hammer to apply a driving force to the top of a pile.

BACKGROUND

For certain construction projects, elongate members such as piles, anchor members, caissons, and mandrels for inserting wick drain material must be placed into the earth. It is well-known that such rigid members may often be driven into the earth without prior excavation. The term "piles" will be used herein to refer to the elongate rigid members typically driven into the earth.

One system for driving piles is conventionally referred to as a diesel hammer. A diesel hammer employs a floating ram member that acts both as a ram for driving the pile and as a piston for compressing diesel fuel. Diesel fuel is injected into a combustion chamber below the ram member as the ram member drops. The dropping ram member engages a helmet member that transfers the load of the ram member to the pile to drive the pile. At the same time, the diesel fuel ignites, forcing the ram member and the helmet member in opposite directions. The helmet member further drives the pile, while the ram member begins a new combustion cycle. Another such system is a drop hammer that repeatedly lifts and drops a hammer onto an upper end of the pile to drive the pile into the earth.

Diesel hammers seem to exhibit fewer problems with tension cracking in concrete piles than similarly configured external combustion hammers. The Applicants have recognized that the combustion chambers of diesel hammers preload the system before the hammer impact and that this preloading may explain the reduction of tension cracking in concrete piles associated with diesel hammers.

The need thus exists for improved drop hammers that induce stresses in the pile driven that are similar to the stresses induced by diesel hammers.

SUMMARY

The present invention may be embodied as a drop hammer for driving a pile comprising a ram member and a lifting system. The ram member is supported within a housing chamber for movement relative to the housing member between the lower position and the upper position. The lifting system moves the ram member from the lower position to the

upper position. When the lifting system raises the ram member above a preload position, ambient air substantially freely flows into and out of the housing chamber through a vent port. When the ram member falls below the preload position, fluid is prevented from flowing through the vent port such that ambient air within a preload chamber portion of the housing chamber compresses to create a preload force that is transmitted to the pile. When the ram member moves into the lower position, an impact force generated by the ram member is transmitted to the pile.

The present invention may also be embodied as a method of driving a pile comprising the following steps. A ram member is supported within a housing chamber for movement between an upper position and a lower position. The ram member is raised into the upper position and then allowed to fall from the upper position to the lower position such that the ram member transmits an impact force to the pile. While the ram member is above a preload position, ambient air is allowed to flow substantially freely into and out of the housing chamber through a vent port. While the ram member is below the preload position, fluid from is substantially prevented from flowing through the vent port such that ambient air within a preload chamber portion is compressed to transmit a preload force to the pile prior to transmission of the impact force to the pile.

The present invention may also be embodied as a drop hammer for driving a pile comprising a ram member, a helmet member, and a lifting system. The ram member is supported within a housing chamber for movement between the upper position and the lower position. The helmet member is supported for movement between a first position and a second position. The lifting system raises the ram member from the lower position to the upper position. As the ram member moves between the upper position and a preload position defined by a vent port, ambient air substantially freely flows into and out of the housing chamber through the vent port. When the ram member falls below the preload position and before the ram member contacts the helmet member, fluid is prevented from flowing through the vent port such that ambient air within a preload chamber portion of the housing chamber below the vent port compresses to transmit a preload force to the pile through the helmet member. When the ram member moves into the lower position, the ram member contacts the helmet member such that an impact is transmitted to the pile through the helmet member.

BRIEF DESCRIPTION OF THE DRAWINGS

FIGS. 1A-1E are somewhat schematic sectional views of a drop hammer of the present invention depicting the drive cycle thereof; and

FIGS. 2-4 represent computer simulations of force records comparing a conventional drop hammer with a conventional diesel hammer under various conditions.

DETAILED DESCRIPTION

Turning to the drawing, depicted at **20** in FIGS. 1A-1E is a drop hammer system constructed in accordance with, and embodying, the principles of the present invention. The drop hammer system **20** is designed to insert a pile **22** into the ground. The drop hammer system **20** will include a spotter, crane, or other equipment as necessary to hold the hammer system **20** in a desired orientation with respect to the ground. Such structural components of the hammer system **20** are conventional and will not be described herein.

The drop hammer system 20 comprises a ram member 30, a helmet member 32, a housing member 34, and a clamp assembly 36. The housing member defines a housing chamber 38. The ram member 30 is guided by the housing member 34 for movement within the housing chamber 38 between a lower position (FIG. 1B) and an upper position (FIG. 1D). The helmet member 32 is guided by the housing member 34 for movement between a rest position (FIG. 1A) and an impact position (FIG. 1B). The helmet member 32 is rigidly connected to the clamp assembly 36. The clamp assembly 36 is detachably fixed relative to the pile 22.

A preload chamber portion 40 is formed within the housing chamber 38 of the housing member 34 between a lower surface 42 of the ram member 30 and an upper surface 44 of the helmet member 32. The ram member 30 further defines an outer surface 46, while the helmet member 32 defines an outer surface 48. First and second seals 50 and 52 are arranged in first and second gaps 54 and 56 between an inner surface 46 of the housing member 34 and the outer surface 46 of the ram member 30 and outer surface 48 of the helmet member 32, respectively. When the seals 50 and 52 function properly, fluid is substantially prevented from flowing out of the preload chamber portion 40 through the gaps 54 and 56 under certain conditions.

In particular, a vent port 60 is formed in the housing member 34. The vent port 60 is arranged to allow exhaust gasses to be expelled from the preload chamber portion 40 under certain conditions and to allow air to be drawn into the chamber 40 under other conditions. The vent port 60 thus defines a preload position above which fluid can flow into and out of the preload chamber portion 40 and below which the preload chamber portion 40 is substantially sealed.

FIG. 1 illustrates a latch assembly 70 that moved up and down as will generally be described below. The latch assembly 70 represents an external lifting system that lifts the ram member 30 from the lower position to the upper position. The latch assembly 70 mechanically latches onto the ram member 30 during lifting and releases from the ram member 30 when the ram member reaches its upper position. The latch assembly 70 and external lifting system are well-known in the art and will not be described herein in detail.

The drop hammer system 20 operates in a drive cycle that will now be described with reference to FIG. 1. Referring initially to FIG. 1A, the hammer system 20 is shown in a preload state. In the preload state, the ram member 30 has dropped past the vent port 60 such that the first seal 50 prevents fluid from flowing out of the preload chamber portion 40. The second seal 52 seals the opposite end of the preload chamber portion 40 as generally described above. Accordingly, at this point the preload chamber portion 40 is effectively sealed, and continued dropping of the ram member 30 compresses the fluid within the preload chamber portion 40. During this preload state, the helmet 32, the clamp assembly 36, and the pile 22 are gradually forced together by the compressed fluid in the preload chamber portion 40.

Referring now to FIG. 1B, the hammer system 20 is shown in an impact state in which the lower surface 42 of the ram member 30 contacts the upper surface 44 of the helmet member 32. In the impact state, the ram member 30 drives the helmet member 32 towards the pile 22 relative to the housing member 34 as shown by a comparison of FIGS. 1A and 1B. The helmet member 32 thus drives the pile 22 downward through the clamp assembly 36. In addition, the housing member 34 will immediately fall onto the helmet member 32, thereby applying additional driving forces onto the pile member 22.

After impact, the helmet member 32 is raised to an upper position as shown in FIG. 1C. As the helmet member 32 moves into the upper position, the lower end of the ram member 30 passes the vent port 60. As the ram member continues on to its upper position, ambient air is drawn into the preload chamber portion 40 through the vent port 60, thereby reducing resistance to continued upward movement of the helmet member 32. As generally described above, the ram member 32 is raised by the latch assembly 70, which is in turn driven by an external combustion source in a manner similar to that of a conventional drop hammer. In addition or instead, a hydraulic actuator may be used to raise the latch assembly 70 and ram member 32.

After the ram member 30 reaches the upper position as shown in FIG. 1D, the latch assembly 70 releases and the ram member 30 is allowed to drop again. The system 20 then enters a free-fall state as shown in FIG. 1E. In the free-fall state, the preload chamber portion 40 is not sealed, and air is allowed to escape through the vent port 60, again reducing resistance to downward movement of the ram member 32. As the ram member 30 continues to drop, the first seal 50 on the ram member 32 again passes the vent port 60, which seals preload chamber portion 40. Again, the system 20 enters the preload state as described with reference to FIG. 1A. At this point, and the drive cycle begins again.

Given the foregoing general discussion of the invention, certain aspects of the exemplary hammer system 20 will now be described in further detail. The helmet member 32 comprises an inner portion 80 that lies within the preload chamber portion 40, a connecting portion 82 that extends through a helmet opening 84 formed in a bottom wall 86 of the housing member 34, and an outer portion 88 that is connected to the clamp assembly 36. The length of the connecting portion 82 (i.e., the distance between the inner portion 80 and outer portion 88) defines the range of movement of the helmet member 32 between the rest position and the impact position. The second seal 52 is formed on the inner portion 80 of the helmet member 32.

The theoretical benefits of preloading the system by compressing fluid prior to impact will now be described with reference to FIGS. 2-4. FIGS. 2, 3, and 4 plots computer generated models illustrating force versus time for various diesel and drop hammer configurations.

FIG. 2 illustrates the difference between a diesel hammer and a conventional drop hammer. The plot of FIG. 2 assumes the following conditions: 12" square concrete pile 400' in length with a three-inch thick plywood pile cushion; the pile was embedded 20 feet with a total soil resistance of 100 kips. The 400' pile length is not realistic but illustrates wave compression at the upper end of the pile without the effects of reflected waves. Trace 90a corresponds to the force record of an American Piledriving Equipment D-19-32 diesel hammer, while trace 92a corresponds to a conventional drop hammer of similar geometry and weight under the same conditions.

The trace 90a illustrates that the force during the time corresponding to a first time second Aa in FIG. 2 is the pile top force caused by the diesel hammer pre-compression force. In the first time sector Aa, the ram has moved past the exhaust ports and is compressing the air in the combustion chamber and thereby exerting a force on the pile. Impact occurs at first time point P1a at the end of the first time sector Aa. The impact exerts an impact force during a second time sector Ba between the first point P1a and a second time point P2a. This second sector Ba represents the force at the top of the pile from the time of impact to the time of ram separation. During this second time sector Ba, pile penetration is induced by the large force arising from ram impact. Somewhere around the

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second time point P2a, the ram has separated from the impact block. A third time sector Ca begins at the second time point P2a; the third time period corresponds to the period from ram separation to the arrival of the reflection of the impact wave back from the toe of the pile. The force during this time comes from the combustion chamber pressure.

The force associated with the conventional drop hammer is shown by the trace 92a. The trace 92a illustrates that the stroke is set such that the same peak impact force was obtained. The double humped force record in sector Ba associated with impact is likely due to the dynamic interaction of the ram, pile cushion, and helmet. While a similar effect is associated with trace 90a in sector Ba, the effects of the dynamic interaction of the ram, pile cushion, and helmet are likely smoothed by the combustion chamber pressure. After the impact as shown at P1a, the drop hammer force stays near zero during the third time sector Ca.

The relatively slow decay of the induced force after the impact event associated with the diesel hammer trace 90a provides a compression force that acts to reduce the magnitude of any reflected tension stresses. The downward traveling compression wave associated with the trace 90a reduces the reflected tension wave from the pile toe.

FIG. 3 illustrates a more realistic example using a conventional diesel hammer system to drive a pile having a length of 100; all other conditions are also the same. As shown by trace 90b, the element with the largest tension stress was located about 30 feet from the top of the pile. The maximum tension force at point 3 in FIG. 3 was 106 kips or 736 psi.

FIG. 4 contains a trace 92c of a conventional drop hammer. Illustrated at point 1 on the trace 92c in FIG. 4 is element with the largest tension stress. This element is about 30 feet from the bottom of the pile and represents a maximum tension force of approximately 166 kips or 1,140 psi. The tension force associated with the trace 92c is thus significantly larger than that represented by the trace 90b.

Given the foregoing, the Applicants have concluded that the operation of conventional drop hammer systems can be improved by establishing a pre-load state prior to impact that is generally similar to the compression state of a diesel hammer. The Applicants believe that the preload state will stretch out the compression force in the stress wave and thereby substantially reduce the possibility of tension cracking and damage in concrete piles.

What is claimed is:

1. A drop hammer for driving a pile comprising:

a ram member supported within a housing chamber for movement relative to the housing member between the lower position and the upper position;

a lifting system for moving the ram member from the lower position to the upper position; and
a helmet member; whereby

when the lifting system raises the ram member above a preload position, ambient air substantially freely flows into the housing chamber through a vent port;

when the lifting system releases the ram member from the upper position,

the ram member moves from the upper position towards the preload position, and

the ram member forces a first portion of ambient air within the housing chamber out of the housing chamber through the vent port;

when the ram member falls below the preload position, the ram member compresses a second portion of the ambient air within a preload chamber portion of the housing chamber, where compression of the second portion of

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the ambient air within the preload chamber creates a preload force on the helmet member that is transmitted to the pile;

when the ram member falls into the lower position, the ram member strikes the helmet member to generate an impact force that is transmitted through the helmet member to the pile; and

seal system for sealing the preload chamber portion of the housing chamber when the ram member is below the preload position.

2. A drop hammer as recited in claim 1, in which the helmet member is supported for movement between a first position and a second position, where the helmet member transmits the preload force and the impact force to the pile.

3. A drop hammer as recited in claim 2, further comprising: a housing member for defining the housing chamber, where the housing member supports the helmet member for movement relative to the housing member between the first position and the second position; wherein the helmet member extends through a helmet opening formed in the housing member.

4. A drop hammer as recited in claim 3, in which:

the ram member defines a ram side wall;

the housing member defines a housing interior wall;

fluid flow between the ram side wall and the housing interior wall is inhibited.

5. A drop hammer as recited in claim 1, further comprising a clamp assembly for securing the helmet member to the pile.

6. A method of driving a pile comprising:

supporting a ram member within a housing chamber for movement between an upper position and a lower position;

supporting a helmet member relative to the ram member such that the ram member contacts the helmet member when in the lower position;

raising the ram member into the upper position;

allowing the ram member to fall from the upper position to a preload position such that the ram member forces a first portion of ambient air within the housing chamber out of the housing chamber through a vent port;

allowing the ram member to continue to fall from the preload position to the lower position such that the ram member compresses a second portion of the ambient air within a preload chamber portion of the housing chamber;

allowing the ram member to strike the helmet member to generate an impact force that is transmitted through the helmet member to the pile; and

inhibiting fluid flow between a side wall of the ram and an interior wall of the housing.

7. A method as recited in claim 6, further comprising the steps of:

providing a housing member defining the housing chamber and the upper and lower positions; and

forming the vent port between in the housing member between the lower and upper positions, where the vent port defines the preload position.

8. A method as recited in claim 7, further comprising the steps of:

supporting the helmet member for movement between a first position and a second position; and

transmitting the preload strength and the impact force to the pile through the helmet member by displacing the helmet member from the first position to the second position when the ram member strikes the helmet member.

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9. A method as recited in claim 8, further comprising a clamp assembly for securing the helmet member to the pile.

10. A method as recited in claim 6, further comprising the step of sealing the preload chamber portion of the housing chamber when the ram member is below the preload position.

11. A drop hammer for driving a pile comprising:

a ram member supported within a housing chamber for movement between the upper position and the lower position;

a helmet member supported for movement between a first position and a second position; and

a lifting system for raising the ram member from the lower position to the upper position; whereby

as the ram member moves between the upper position and a preload position defined by a vent port, the ram member forces a first portion of ambient air within the housing chamber out of housing chamber through the vent port;

when the ram member falls below the preload position and before the ram member contacts the helmet member, the ram member compresses a second portion of the ambi-

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ent air within a preload chamber portion of the housing chamber below the vent port, where compression of the second portion of the ambient air within the preload chamber creates a preload force that is transmitted to the pile through the helmet member;

when the ram member moves into the lower position, the ram member contacts the helmet member such that an impact is transmitted to the pile through the helmet member; and wherein

the ram member defines a ram side wall;

the housing member defines a housing interior wall;

a ram seal inhibits fluid flow between the ram side wall and the housing interior wall.

12. A drop hammer as recited in claim 11, further comprising a housing member defining the housing chamber and the vent port, where the housing member supports the ram member and the helmet member.

13. A drop hammer as recited in claim 11, further comprising a clamp assembly for securing the helmet member to the pile.

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